Geoelectrical Investigation of Soil Corrosivity and Aquifer Protective Capacity in Angware and Its Environs, Jos-Plateau, Northcentral Nigeria

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Abstract

Geoelectrical resistivity method was adopted in the study of soil corrosivity and aquifer protective capacity (APC) in Angware and its environs, Jos-Plateau. This present study focuses on delineating zones that are very prone to groundwater contamination from surface contaminants and subsurface soils that are corrosive to utility pipes. Seventy-four (74) vertical electrical sounding (VES) stations were occupied in Angware and Its Environs with current spacing (AB/2) ranging from 1 to 125 m using Schlumberger array. ABEM SAS 300C terrameter was used to generate the data. The interpretations of the VES data were supported by WinResist, Excel and surfer software. The geoelectric sections indicate four (4) layers which include: topsoil, clayey layer, fractured basement and fresh basement while two (2) major aquiferous units identified were weathered basement and fractured basement with thickness of 11.30 to 41.07 m. Topsoil resistivity values were adopted in classification of soil corrosivity and four zones of soil corrosivity were recognized in the area namely: very strongly corrosive zone (< 10 Ω m), moderate corrosivity zone (10 - 60 Ω m), slightly corrosivity zone (60 - 180 Ω m) and practically noncorrosive zone (> 180 Ω m). The value of longitudinal conductance of the overburden units varies from 0.008523 to 1.829263 mhos and four (4) aquifer protective capacity zones were delineated based on the longitudinal conductance values namely: poor (< 0.1 mhos), weak (0.1–0.19 mhos), moderate (0.2–0.69 mhos) and good (0.7–4.49 mhos). The poor and weak aquifer protective capacity zones have higher protection against surface contamination, while the good and moderate aquifer protective capacity zones have higher protection against surface contamination are apparently safe.

Keywords: Overburden, Geoelectric, corrosivity, protective and aquifer.

Introduction

Groundwater encompasses water that exists in the subsurface and is contained in geologic formation called aquifers. Aquifers are geological formations that are porous and permeable which retained and released water (Wightman et al., 2003; Todd and Mays, 2005). The soils and rocks resistivities depend largely on properties of rocks which include permeability, soil porosity, ionic value of the pore fluids, and clay mineralization and these differ with time and space (Oseji, 2010). Geophysical techniques have been applied for groundwater contamination studies (Kelly, 1976; Benson et al., 1997; Arristodemou and Thomas-Betts, 2000; Adepelumi et al., 2001; Naudet et al., 2004). Geoelectrical methods were developed to demarcate locations prone to contamination (Braga et al., 2006; Atakpo and Ayolabi, 2009; Mogaji et al., 2007; Abiola et al., 2009).

Angware area occurs in Jos East Local Government Area of Plateau State on Longitudes 9.09095° to 9.13888°E and Latitudes 9.97981° to10.01461°N (Fig. 1). Angware area is located in the Guinea Savannah region with scattered trees and is typified by wet and dry seasons. The Geological setting of the study area is characterized by basement rocks namely: migmatite, fine to medium-grained biotite and biotite muscovite granite and Neil's Valley granite porphyry (Figure 2). survey involving 1-D VES readings. Seventy-four (74) VES stations were occupied in Angware area and ABEM SAS 300C terrameter was used to generate the data. The coordinates of the VES station was taken with the Garmin handheld Global Positioning System (GPS) device for longitude and latitude readings while the data

sheet was used for recording field data.

Due to the increasing population of Angware area, industrial and domestic wastes were being generated

which may contaminate the groundwater. This present

study focuses on delineating zones that are very prone to

groundwater contamination from surface contaminants

and subsurface soils that are either corrosive or non-

Schlumberger electrode array with half-current

electrode separation (AB/2) ranging from 1 to 125 m

was adopted in the field measurements and geoelectrical

corrosive to utility pipes.

Materials and Methods

Resistivity data were inverted using WinResist software program and was design to avoid the curve-matching method. Filed data were uploaded into the program window and the software generates a curve of apparent resistivity plotted against electrode separation (AB/2). An inversion was then run until a perfect match was obtained and necessary monitoring of the process must be ensured for precision. The total longitudinal



Fig. 2: Geological map of Angware and environs.

conductance (S) of Angware and environs was estimated from equation after Zohdy *et al.*, (1974)

$S = \Sigma (hi/\rho i) = h1/\rho 1 + h2/\rho 2 + ... + hn/\rho n$

Where S is the total longitudinal conductance,

 Σ is summation sign,

hi is thickness of the nth layer and ρ **i** is resistivity of the nth layer.

Results

The values of layer resistivity and layer thickness obtained from the seventy-four (74) VES stations are presented in Table 1. The curve types, longitudinal conductance values and aquifer thickness are also presented in Table 1. The sounding curves found within the study area have 3-layer model (A, H and Q); 4-layer model (AA, HA, HK, KH, QH and QQ) and 5-layer model (HAA) of geoelectrical layers (Table 1). The geoelectric section ranges from 3 to 5 layers with the 3-layer as the dominant type (Table 2). Figure 3 shows the representative VES curves in Angware and its environs which include: Q-curve, QH-curve, HA-curve and AA-curve. Figure 4 shows the frequency of curve type distribution in Angware and its environs.

Discussion

Aquifer Units within the Area

The weathered and fractured zone thickness of Angware and its environs (Figure 5) indicates that the highest thickness of weathered layer unit of about 41.07m was identified at VES 50 and the thickness of the weathered layer unit with the lowest thickness of about 11.3m occurs at VES 71 and VES 73. Thus, the thickness of weathered and fractured layers of Angware and its environs is relatively high for groundwater accumulation. The two (2) aquifer units within the area include the weathered layer and fractured basement. The weathered aquifer (porous and not permeable) is incompetent, fragile and easily collapse when drill hole is left without support inside it while the fractured basement aquifer is competent and permeable. The two aquifer types are connected together with the weathered aquifer overlying the competent fractured basement aquifer.

Evaluation of Soil Corrosivity

The thickness of the topsoil layer varies from 0.5 to 17.4 m and the resistivity varies from 9.2 to $3257.4\Omega m$. The topsoil resistivity values obtained from the study area (Table 1) was adopted in the interpretations and evaluation of the corrosivity as shown in Figure 6. Topsoil resistivity values were used in the classification of soil corrosivity based on the classification of Baeckmann and Schenwenk (1975); Agunloye (1984) and Oladapo *et al.* (2004). The low topsoil resistivity values ranging from 10 to 60 Ωm denotes moderate corrosivity zones while the topsoil resistivity values ranging from 60 to 180 Ωm represents slightly corrosivity zones and areas with resistivity values of > 180 Ωm indicates practically noncorrosive (Figure 5).

Evaluation of Aquifer Protective Capacity

The values of longitudinal conductance were adopted to classify overburden units into good, moderate, weak and poor aquifer protective capacity zones based on the classification of Henriet (1976) and Oladapo *et al.* (2004). The longitudinal conductance of 0.7 to 4.9 mhos indicates good aquifer protective capacity and longitudinal conductance of 0.2 to 0.69 shows moderate aquifer protective capacity while longitudinal conductance of 0.1 to 0.19 mhos indicates weak aquifer protective capacity. The highest longitudinal conductance value of 1.829263 mhos was identified at VES 21 and lowest longitudinal conductance value of 0.008523 mhos was identified at VES 16 (Table 1).

The good and moderate aquifer protective capacity zones coincide with zones of considerable overburden thicknesses with high clay column and low resistivity value while the weak and poor zones coincide with zones of shallow or thin overburden thickness and high electrical resistivity value. Yellow and powder blue colours areas are covered by poor and weak Aquifer protective capacity zones and they may be vulnerable to surface contamination sources such as leakage from underground petroleum storage tanks, infiltration of leachates from decomposing of open refuse dumps and diffuse pollution from agricultural activities within the study area (Figure 7).

The good (pink colour) and moderate (cyan colour) aquifer protective capacity zones of the study area have higher protection against surface contaminated fluids so that in the face of contamination such zones are apparently safe (Figure 7). High total longitudinal

	Resistivity (Ohm-m)					Thickness (m)				Longitudinal	Aquifer	
VES	A .	0.	. <u>.</u>	<i>c</i> .	0-	þ.	R.	h.	ь.	Curve	Conductance	Thickness
Station	P1	ρ_2	<i>p</i> ₃	P4	ρ_5	п1	n ₂	Цэ	П4	Туре	(mhos)	(m)
1	490.6	207.7	250			5.2	30			Q	0.155038	36.47
2	381.2	113.7	82.2			3.1	19,1			Q	0.176118	38,57
3	340.2	78.4	109.8			1.9	33.6			H	0.434156	39.77
4	424.5	169.8	130			9.0	20			Q Q	0.138997	32.67
5	300.8	212.0	192.2			2.0	14.7			Q U	0.077814	39.07
7	572.4	312.2	776.5			2.0	71			0	0.180945	30.67
8	488.7	204.6	870			2.6	44.8			õ	0.224284	39.07
9	292.1	65.7	374.3			1.3	34			Ř	0.521954	40.37
10	748.2	211.4	23.2	574.1		1.1	8.1	19.4		OH	0.875993	40.57
11	453.1	239.7	95.1	536,5		1.4	9.7	26.0		QH	0.316954	40.27
12	343.6	245.1	104.2			1.3	8.4			Q	0.038055	40.37
13	702.2	128.0	50.2			0.8	6.9			Q	0.055046	40.87
14	933.9	239.8	162.7			3.6	20.2			Q	0.088092	38.07
15	656.9	335.1	254.7			3.2	7.1			Q	0.026059	38.47
16	2218,1	456.0	1113.8	183,9		1.1	1.9	4,3		HK	0.008523	34,27
17	372.2	122.2	698.0	105.0		2.9	26.3			H	0.16463	38.77
18	162.2	/63.9	81.6	195.0		4.9	3.2	/.6		KH OU	0.103755	36.77
19	900 4	100.1	37.4	393,4		8.5	4.8	21,6		QH	0.619203	33.17
20	899.0	460.4	104.4			1.5	9.0 56 1			à	1 820263	40.37
77	3257.4	737.5	65.8	244.6		1.5	5.5	47.0		он Он	0.661916	39.47 40.17
23	935 7	200.8	41.5	7161		17	75	137		OH	0 369288	39.97
24	2793.8	1328.0	229.5	158.8		0.6	6.6	2.7		00	0.016949	37.07
25	352.7	278.6	38.9	553.3		3.6	3.4	13.9		QH	0.379737	38.07
26	331.2	109.5	1501.4			1.7	28,3			Ĥ	0,26358	39.97
27	104.1	44.0	596.1			1.2	30.9			Н	0.7138	40.47
28	434.5	184.8	44.2			2.8	23.6			Q	0.13415	38.87
29	444.6	198.0	28.0	887,3		2.5	3.2	12.0		QH	0,450356	39.17
30	1015.1	262.2	232.0	293.1		2.0	2.5	12.7		QH	0.066246	39
31	296.6	70.3	704.5	0414.5		1.7	10.2	0.5		H	0.13415	39.97
32	115.4	48.1	147.0	2614.5		0.6	13.5	8.5		HA	0.103755	22.6
33	1284.0	4/.0	334.7	1000.4		0.6	24.2	16.0			0.509138	41.07
34	049 7	500.4	1778	147.8		27	0.9	2.6		OU	0.343967	27.7
36	138.4	310.7	14410	147,0		115	116	3,0		A	0.110433	23 1
37	47.5	91.0	288.6	6153		11.4	75	197		AA	0.390678	38.27
38	564.9	32.2	137.3	1335.8		0.5	5.0	18.0		HA	0.287264	23.5
39	185.3	87.1	265.3	830,9		1.9	3.0	15.7		HA	0,103875	39,77
40	229.8	70.3	2701.2			2.5	18.9			н	0.279727	21.4
41	808.4	131.1	57.2	2659.2		1.6	3.5	14.3		QH	0.278676	19.4
42	280.5	71.0	570.8			1.6	13.9			Н	0.201479	40.07
43	18.0	79.1	928.7			0.8	31.4			Α	0.44141	40.87
44	264.4	116.0	1317.2			0.8	25.2			H	0.220267	26
45	912.0	112.3	19.8	992.7		0.8	1.0	13.0		QH	0.666348	40.87
46	783.5	218,2	24.3	1443.6		0.8	4.8	9.6		QH	0,418081	15.2
47	34.1	30.8	16.0	129.2		1.8	20.5	14.0		Q VV	0.282780	39.8/
40	20.0	33.2	260.5	126.5		5 2	16.0	14.9		A	1.047483	3637
50	100 4	295	593	611.3		0.6	31	25 û		НА	0 544856	41.07
51	169.3	100.6	89.9	673.6		2.6	13.1	23.4		OH	0.405865	39.07
52	129.2	39,2	580.6	85.5		1.8	4.5	25.9		HK	0,173337	39.87
53	106.3	170.4	35.9	254,3		2.9	4.4	17.0		КН	0.52664	38.77
54	267.7	50.3	355.9			3.2	30,0			н	0.608375	38.47
55	101.3	90.1	27.1	320.7		2.7	3.8	15.6		QH	0.644475	38.97
56	181.3	88,7	60.0	636,9		1.4	11.0	18.8		QH	0.445069	40.27
57	23.1	1802.0	2100.0			17.4	20			Α	0.764346	17.4
58	460.8	32.6	36.0	1056.5		1.0	8.2	8.9		HA	0.500926	18.1
59	289.1	105.7	116.6			3.6	1.2			н	0.023805	38.07
60	244.2	36.3	540.4	226.2		1.0	20.9	10 4		H	0.579853	40.67
61	187.5	915.5	257.2	220.2		3.6	8.1	19.6		KH	0.104253	38,07
62	231.1	120.0	1535,9			2.8	25,3			н	0.398394	28.1
03 64	443,3	136,8	01.2			2.5	14,9			Ч Ц	0,112311	39.37
65	157.0	63.0	2104.7	378.0		5.8	80	14.2		н	0.374219	35.87
66	438.4	37.8	674	185.0	2818 5	0.6	24	13.6	82	HAA	0.310965	24.8
67	35.5	13.4	138.4	3009.4	2010.3	1.0	7.1	6.4	0.2	HA	0.604263	14.6
68	23.5	113.6	360.7	1747.7		4.5	4.6	10.3		AA	0,260538	19,4
69	389.6	88.1	235.2	148.5		2.3	3.6	25.8		HK	0.15646	39.37

3.6 14.2 3.7 18.6 10.1 6.3 314.7 1.3 46.1 QH VES = vertical electrical sounding, ρ_1 = first-layer resistivity, ρ_2 = second-layer resistivity, ρ_3 = third-layer resistivity, ρ_4 = fourth-layer resistivity, ρ_{s} = fifth-layer resistivity, \mathbf{h}_{i} = first-layer thickness, \mathbf{h}_{2} = second-layer thickness, \mathbf{h}_{3} = third-layer thickness, \mathbf{h}_{4} = fourth-layer thickness, \mathbf{m} = meters.

2.3 1.5 1.2 1.0 1.2

6.4

Н

HA A H

40.17

11.3 19.6 11.3

40.37

0.13046 0.063079 0.100941 0.48883 0.248163

0.393161

88.1 235.2

42.4 44.3 41.3

253.2

408.5

834.3 2694.0 3761.7

125.9

3333.8

554.5 199.8 14.5 332.3

614.3





Fig. 3: Representative VES curve in Angware and its environs (a) Q curve, (b) QH curve, (c) HA curve and (d) AA curve. Table 2: Qualitative analysis of curve types

S/No	Curve Types	Frequency	Percentage (%)	Layer's resistivity Relationship	Number of geoelectric layers
1	Α	5	6.76	$\rho I < \rho 2 < \rho 3$	3
2	Q	15	20.27	$\rho 1 > \rho 2 > \rho 3$	3
3	Н	18	24.32	$\rho 1 > \rho 2 < \rho 3$	3
4	AA	2	2.7	ρ1<ρ2<ρ3<ρ4	4
5	HA	8	10.81	ρ1>ρ2<ρ3<ρ4	4
6	HK	3	4.06	$\rho I > \rho 2 < \rho 3 > \rho 4$	4
7	KH	4	5.41	ρ1<ρ2>ρ3<ρ4	4
8	QH	17	22.97	$\rho 1 > \rho 2 > \rho 3 < \rho 4$	4
9	QQ	1	1.35	$\rho 1 > \rho 2 > \rho 3 > \rho 4$	4
10	HAA	1	1.35	ρ1>ρ2<ρ3<ρ4<ρ5	5
Total		74	100		

Note: ρ - resistivity

conductance (S) values are indicative of deeper basement while low value of total longitudinal conductance (S) represent shallow basement and an increase in the total longitudinal conductance (S) value may correspond to a typical increase in the clay content and consequently a decrease in the transmissivity of the aquifer (Oteri, 1981; Khali, 2009).

In this study, low values of the total longitudinal conductance (<0 - 0.19 mhos) correspond with deeper basement with comparable thick aquifer units at VES 1, VES 2, VES 4, VES 5, VES 12, VES 13, VES 14, VES



Fig. 4: The frequency of curve type distribution in Angware and its environs



Fig. 5: Aquifer thickness map of Angware and environs



Fig. 6: Soil corrosivity map of Angware and its environs with VES location

15, VES 16, VES 17, VES 18, VES 20, VES 24, VES 28, VES 30, VES 35, VES 59, VES 63, and VES 70. This inconsistency could only come from the differences in geologic terrain and is in contrast with report of Oteri (1981) in sedimentary area. The study also revealed high values of total longitudinal conductance (0.20 - 1.829263 mhos) as shown in Table 1 with thick aquifer devoid of clay layer above it at VES 8, VES 10, VES 11, VES 19, VES 21, VES 22, VES 23, VES 25, VES 29, VES 45, VES 53 and VES 74 (Figure 8). Hence, the absent of clay content over the aquifer will increase its transmissivity and render it susceptible to surface fluid contaminants (Adeniji *et al.*, 2014).



Fig. 7: Longitudinal Conductance map of Angware and environs



Fig. 8: A graph of Longitudinal Conductance map of Angware and environs

Geo-Electric Sections

The 2-D geoelectric sections (Figs. 9a - c) were all plotted in the north-south directions along A-A, B-B and C-C Profile lines (Figure 1). Three (3) distinctive geoelectric layers were identified in A-A profile section as shown in Figure 9a. The topsoil has resistivities of 340.2 to 720.9 ohm-m and thickness values of 1.90 to 10.80 m. The second layer consists of clay/fractured basement with resistivities value of 78.4 to 94.6 Ohm-m and thickness of 15.7 to 33.6 m. The very thick clay layer underlying the topsoil was observed at VES 3 and VES 6 while the fractured basement across the section was located at VES 1, VES 2, VES 4, VES 5 and VES 7 with their resistivities value of 113.7 to 312.2 ohm-m and thickness of 7.1 to 30 m. The third layer consists of fractured basement with resistivities of 82.2 to 424.9 ohm-m and an infinite depth. This A-A profile has very thick aquifer (Fig. 9a) and is good for groundwater production with the exclusion of VES 3 which has a thick clay layer. Oteri (1981) and Khali (2009) reported that an increase in the clay content will decrease the transmissivity of the aquifer and render it unproductive for groundwater production.

Four (4) distinct geoelectric layers were identified in B-B profile section as shown in Figure 9b. The topsoil resistivities value of 115.4 to 1284 Ohm-m and thickness of 0.6 to 11.5 m. The second layer consists of clay with resistivities of 48.1 to 70.3 Ohm-m and thickness of 10.2 to 24.2 m. The third layer consists of fractured/fresh basement, the fractured basement is superimposed by clay layer at VES 31, VES 32 and VES 33 across the section with resistivities of 28 to 704.5 Ohm-m and thickness of 3.6 to 16.9 m while the fresh basement is located only at VES 36 having resistivity value of 1441.9 Ohm-m with an infinite thickness. The fourth layer consists of fractured/fresh basement, VES 29, VES 30 and VES 35 constitute the fractured basement having resistivities of 147.8 to 887.3 Ohm-m with an infinite thickness, while the fresh basement underlies VES 32 and VES 34 with an unlimited thickness. The aquifer thickness at VES 32 and VES 36 are not thick enough to support groundwater production.

Four (4) distinct geologic layers were identified along the C-C Profile as shown in Figure 9c. The topsoil resistivities range from 35.5 to 761.6 ohm-m with thickness of about 0.6 to 5.8 m. The second laver consists of clay unit underlying the topsoil at VES 64, VES 65, VES 66, VES 67 and VES 69 with resistivities of 13.4 to 88.1 Ohm-m and thickness of 2.4 to 9.6 m. The third layer comprises of fractured/fresh basement with the fractured basement having resistivity of 67.4 to 360 Ohm-m and thickness of 6.4 to 25.8 m while the fresh basement was identified at VES 64 with resistivity of 2164.7 Ohm-m having an infinite thickness. The fourth layer also consists of fractured/fresh basement with the fresh basement underlying VES 66, VES 67 and VES 68 representing the impermeable layer having resistivities of 1747.7 to 3009.4 ohm-m with an inestimable thickness. Only VES 65 and VES 69 were recommended for locating borehole owing to their thick aquifer and clay layer overlying this location in order to prevent contamination from surface fluid infiltration.

Conclusion

The sounding curves show three to five model layers namely: three (3) layer model (A, H and Q); four (4) layer model (AA, HA, HK, KH, QH and QQ); and five (5) layer model (HAA) geoelectric layers with the 3layer model as the dominating type.

The geoelectric sections along the profiles revealed three to four subsurface layers namely: the topsoil, clayey layer, fractured basement and the fresh basement. The two major aquiferous units were the weathered layer and fractured basement.



Fig. 9a: Geoelectric Section along Profile A-A'





The topsoil resistivity values were adopted soil corrosivity classification and four zones of soil corrosivity were recognized in the area namely: very strongly corrosive zone (< 10 Ω m), moderate corrosivity zone (10 - 60 Ω m), slightly corrosivity zones (60 - 180 Ω m) and practically noncorrosive (> 180 Ω m). Four (4) aquifer protective capacity zones were identified in Angware and its environs based on the longitudinal conductance values namely: good, moderate, weak and poor. The good and moderate aquifer protective capacity zones have higher protection against surface contaminated fluids and are apparently safe.

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